

# Filters for Audio Equalizing and Artificial Reverberation

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## 1 Derivation of Linear-Phase FIR Filter for Audio Equalizer

A full derivation on the design of linear-phase FIR filters is given in [1]. Since we have chosen to shape our equalizer by the desired frequency response in terms of Hz. We will index the desired response  $H_r(\delta_f k)$  in which  $\delta_f$  is the frequency sampling resolution.

$$\delta_f = \frac{F_s}{N} \quad (1)$$

$F_s$  is the sampling frequency in Hz, and  $N$  is the number of taps or samples used to implement the filter. We chose to use a symmetric linear-phase FIR filter. We highlight the key equations from [1] (see Table 8.3), with our desired frequency response. We chose to use an  $\alpha = 0$ , and an  $N$  which was even. The resulting desired linear-phase FIR filter response  $h_d(n)$  is shown in (3).

$$G(k) = (-1)^k H_r(\delta_f k), k = 0, 1, \dots, N - 1 \quad (2)$$

$$h_d(n) = h_d(N - 1 - n) = \frac{1}{N} \left\{ G(0) + 2 \sum_{k=1}^{\frac{N}{2}-1} G(k) \cos \frac{2\pi k}{N} \left( n + \frac{1}{2} \right) \right\} \quad (3)$$

Lastly we chose to use a Hamming window,  $w(n)$  (4), for sampling the audio data in order to minimize ripples in the resulting frequency response of our FIR filter.

$$w(n) = 0.54 - 0.46 \cos\left(\frac{2\pi n}{N - 1}\right) \quad (4)$$

Thus, the resulting equalizer FIR linear-phase filter impulse response,  $h(n)$ , is given in (5).

$$h(n) = w(n)h_d(n) \quad (5)$$

## 2 Derivation of Artificial Reverberation Filter

The artificial reverberation (AR) filter has the following impulse response as shown by [2]. Specifically, the impulse response is given in (6).

$$h_r(n) = h_{fir}(n) + h_{irr}(n - n_d) + \delta(n) \quad (6)$$

The impulse response of the FIR filter  $h_{fir}(n)$  has the following form.

$$h_{fir}(n) = \begin{cases} 10^{\frac{-60n}{20Fs(RT+0.001)}}, & \text{if } n = k \text{ floor}\left(\frac{Fs}{RD}\right); k = 0, 1, \dots, k_{max} \\ 0, & \text{otherwise.} \end{cases} \quad (7)$$

The limit for  $k_{max}$  is determined by  $n_d$ , which is dependent on the IIR time delay ( $T_{iir} = 0.160$  seconds) and the desired reverberation time,  $RT$ .

$$k_{max} = \min(n_d, \text{floor}(RTFs)), n_d = \text{floor}(T_{iir}Fs) \quad (8)$$

For the IIR impulse response, all that is required is a scaled, first-order IIR filter with the following z-transform.

$$H(z) = \frac{g_1}{1 + a_1 z^{-1}} \quad (9)$$

The resulting impulse response is given in (10).

$$h_{iir}(n) = \begin{cases} g_1(a_1)^n, & n \geq 0 \\ 0, & \text{otherwise.} \end{cases} \quad (10)$$

Lastly, the IIR coefficients,  $g_1$  and  $a_1$ , are determined by (11), and (12) respectively.

$$g_1 = 10^{\frac{G_1}{20}}, G_1 = \frac{-60T_{iir}}{RT + .001} \quad (11)$$

$$a_1 = \begin{cases} 10^{A_1}, A_1 = \frac{-3 - \frac{G_1}{20}}{\max(0.001, RT - T_{iir})Fs}, & \text{if } a_1 \leq 1 - 2^{-30} \\ 1 - 2^{-30}, & \text{otherwise.} \end{cases} \quad (12)$$

the bound on  $a_1$  is to keep the IIR filter stable. Since we were required to vary  $RT$  from 0 to 5.0 seconds, the .001 term, was used to avoid a divide by 0 error in this implementation.

## References

- [1] John G. Proakis, Dimitris G. Manolakis, *Digital Signal Processing Principles, Algorithms, and Applications*. Prentice-Hall, Inc., 1996. (pp. 630–633)
- [2] Robert L. Stevenson, EE598D – Project #1